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AIRCRAFT AND ARMADENT EXPERIMENTAL ESTABLISHMENT BOSCOMBE DOWN.

> Corsair F Mk. IV KD. 227 (Double Wasp R2800-8W)

Level speed trials with and without water injection.

A.&.A.E.E. ref: 5703,a/8/JNH M.A.P. ref: Res.Air.5461/

M.A.P. ref: Res. Air. 5461/11/ADRDN
Period of tests: 12th - 16th December, 1944.

PECUPTOWED:

progress of issue of report.

Report No. 1st Part of A.A. .. E. E. /814,0

KD. 227 - Carbon monoxide contamination tests.

2nd Part of Report No. A. &. A. E. E. /814.c

control or equipment as tested Action to remedy defects or decisions to accept items not in strict compliance with the specification are matters for decision and action by M.A.P.

coals .

Summary.

The Corsair F Mt. IV differs from Corsair F Mt. II in the following respects:-

(a) The use of water injection.

(b) U.S. Navy glossy blue finish in place of the Standard Britishcamouflago

(c) Different propeller including a change in diameter from 13' 3" to 131 1".

In auxiliary high supercharger gear, the increase of boost from 52.5 ins. Hg to 60 in. Hg. allowed by the use of water injection, was found to give an increase of speed of 20 mph TAS at all heights up to 18,400 ft., the full throttle height at 60 ins. Hg boost. The maximum true airspeed attained was 400 mph (347 knots at 18,400 ft.

Introduction.

The Corsair IV differs from Corsair II, on which performance measurements have proviously been made at this Establishment, by :-

(a) The use of water injection, allowing increased boost pressure and hence greater power.

U.S. Navy glossy blue finish, instead of standard British camouflage. (b)

A different propeller including a change in diameter from 13: 3" to 15: 1". (c)

Level speed performance measurements were made on this aircraft primarily to determine the effect of water injection and secondly to establish the level speed performance of this variant. The results of the tests are given in this part of the Report, together with those of the static position error determination used in the analysis of the results.

proliminary results have been forwarded to MAP in a letter dated January 9th, 1945.

It should be noted that no correction for pitot error has been applied, since the aircraft crashed before this could be determined. It is, however, intended to determine the pitot error on a replacement aircraft, which will shortly arrive at this station. The results of this determination and its effects on the level speeds, quoted here, will be the subject of an addendum to this Report.

Condition of aircraft relevant to tests.

The aircraft was a production Mk. IV Corsair fighter, built 2.1 General. by the Goodyear Corporation and powered by a pratt and Whitney Double Wasp engine (see para, 2.4)

The main

The main features of the aircraft were :-

Hamilton 3-bladed Hydromatic propeller of paddle-blade design (see para. 2.2) Three exhausts on each side of cowling base.

Oil cooler and intercooler intakes at leading edge of port and starboard wing roots.

Armament - 6 x 0.5 ins. Mk. II browning guns, 3 in each wing. Gun ports and ejection chutes sealed.

Acrial mast on nose, midway between cockpit and engine cowling. The W/T acrial ran to a short mast on top of the rudder, with a lead-in to the starboard side of the fuselage about 2 feet behind the cockpit hood.

Rod aerial on top of fuselage approximately \$\frac{1}{3}\$ distance from hood to tail.

Two short rod aerials undermeath fuselage, one at leading edge, and one 3 ft.

further back.

Dock arrestor hook under tail.

Details of the airspeed indicator system are given in para. 2.3 and Fig. 1

The following table gives the principle differences between this aircraft and the Corsair II, the Mark previously tested at this station.

	Propelle				
Aircraft	Propeller dia.	Blade Drg. No.	Surface finish		
Corsair IV KD. 227	131 1"	6541A - D (paddle-type)	U.S. Navy glossy blue finish		
Corsair II JT.417 and JT.259	131 3"	6443A - 21	Standard British camouflage		

Care was taken throughout the tests to maintain the high polish of the wings and to remove any dirt which might accumulate. No uneveness or distortion of the leading edge or surfaces of the wings was perceptible. As usual, however, with gorsair aircraft, the edges of the insepction panels were bevelled and consequently a small groove surrounded each panel.

2.2 propeller details. Main details were :-

Type No. 23E50-495 Hamilton Hydromatic 131 1" Diameter 3 No. of blades Right hand Direction of rotation 66885 Hub Serial No. 245762 Blade No. 1 Serial No. 245763 245764 Hollow steel. Construction

- 2.3 Airspeed indicator system. The pitot and static sides of the airspeed indicator were connected to a Kollsman pressure head, type AN. 5816-2, which was mounted on the leading edge of the port wing tip (see Fig. 1).
- 2.4 Engine numbers and limitations. The aircraft was powered by a Pratt and Whitney engine R2000-8W (Makers No. HP206106).

The relevant engine limitations applicable to auxiliaty high supercharger gear at the time of test were :-

Max. for level flight at combat power 2700 Manifold pressure in. of Hg. 2700 52.5 without water injection 2700 60 with do.

2.5 Loading. The take-off weight for these trials was 12,080 lb. (no external load carried), and the c.g. was 100.2 in. aft of the axis of reference.

Scope of tests.

3.1 position error. The static position error was measured by the ameroid method in level flight, with flaps and undercarriage up over a speed range of 120 mph ASI to 320 mph ASI.

Those tests were undertaken for use in the reduction of the level speed

3.2 Level speed. Level speeds were measured with engine cowling gills, intercooler shutter and oil cooler shutter closed at heights between 10,000 and 24,000 ft. in auxiliaty high supercharger gear, both with and without water injection.

4. Results of tests.

The results have been corrected to standard atmpspheric conditions by the methods of A.&.A.E.E./Res/170.

Both level speed and position error correction results have been corrected to 11,500 lb. (95% of take-off weight). The compressibility correction has been determined by the method of Report No. A.&. A.E.E./Res/208.

4.1 Position error. The static position error correction varied from +1 mph at 120 mph ASI to +9.7 mph at 320 mph ASI. Full details are given in Fig. 2.

Correction curves for the altimeter when connected to the static side of the airspeed indicator system are given in Fig. 3.

4.2 Level speed. Results of the level speed tests are given in Table I and Fig.4.

The maximum true airspeeds attained were :-

with water injection without water injection

400 mph (347 knots) at 18,400 ft. 395 mph (343 knots) at 22,500 ft.

At all heights up to 18,400 ft. an increase of speed of 20 mph (17.4 knots)
TAS was obtained by the use of the increased boost with water injection.

4.3 Propoller tip Mach number. The highest propeller tip Mach numbers obtained were :-

Meight	Mach No.	Remarks.
18,400	1.04	FTH with water injection
22,500	1.06	FTH without water injection.
24,000	1.06	Highest altitude reached.

As the aircraft crashed, it was not possible to investigate the effect of decreasing rpm (and hence Mach number) on the level speed performance.

The differences in temperature from ICAN standard values were within the ranges given below:

10,000 ft. to 15,000 ft. -2 to +1 °C 15,000 ft. to 20,000 ft. -7 to +0.5 °C 20,000 ft. to 24,000 ft. -6 to -3 °C

5. Comparison with previous results.

The following table gives a comparison of the performance of this aircraft with that of Corsair II JT.417. reported in the 12th Part of Report No. A.&.A.E.E./814,a.

Aircraft	Max. speed without water injection. mph (knots)		95% take-off weight lbs.		
Corsair II JT.417	393 (341)	23,400	The second second		
Corsair IV KD. 227	395 (343)	22,500	11,500		

H 2700 rpm, 52.5 in. Hg. manifold pressure.

This comparison is intended merely to demonstrate the approximate agreement in level speed performance between the two variants.

TABLE I.

Corrected to 95% of the take-off weight - viz. to 11500 lb.
Engine cowling gills, intercooler shutter, and oil cooler shutter closed.

Standard					Corr	ections	Manifold	0	
height	TA		ASI		PE	CE	pressure	RPM	S/c
ft.		knots)			mph	mph	in. of HE,		gear
10,000	349	(303)	300	1	9.0	-3.2	52.5	2700	Aux. high
12,000	356	(309)	296	(257)	9.0	-3.8	20		(without
14,000	363	(315)	293	(255)	8.9	-4.4	1		water in-
16,000	371	(322)	289	(251)	8.8	-4.9			jection)
18,000	378	(328)	285	(248)	8.7	-5.4			
20,000	385	(334)	281	(244)	8.6	-5.9			
22,000	392	(341)	277	(241)	8.5	-6.5			
*22,500	395	(343)	276	(240)	8.5	-6.6	V		V
24,000	393	(341)	268	(233)	8.2	-6.7	49.8		Aux. high(wit & without)
10,000	369	(321)	317	(275)	19.4	-3.7	60		Aux, high
12,000	376	(327)	313	(272)	9.4	-4.4			(with water
14,000	384	(334)	309	(268)	9.3	-5.1		1	injection)
16,000	391	(34.0)	305	(265)	19.2	-5.7			
18,000	398	(346)	300	(261)	9.2	-6.4			
18,400	400	(347)	299	(260)	19.2	-6.6	V		
20,000	398	(346)	291	(253)	8.9	-6.6	54	1	
22,000	395	(343)	279	(242)	8,61	-6.7	53.5	V	V

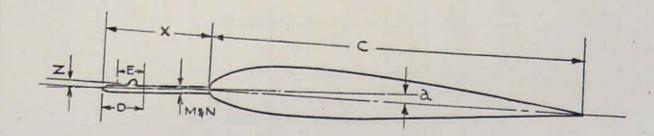
Full throttle heights.

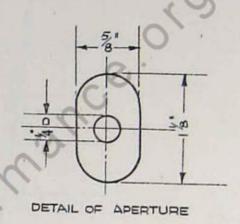
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PRESSURE HEAD POSITION

(L.E. WING)

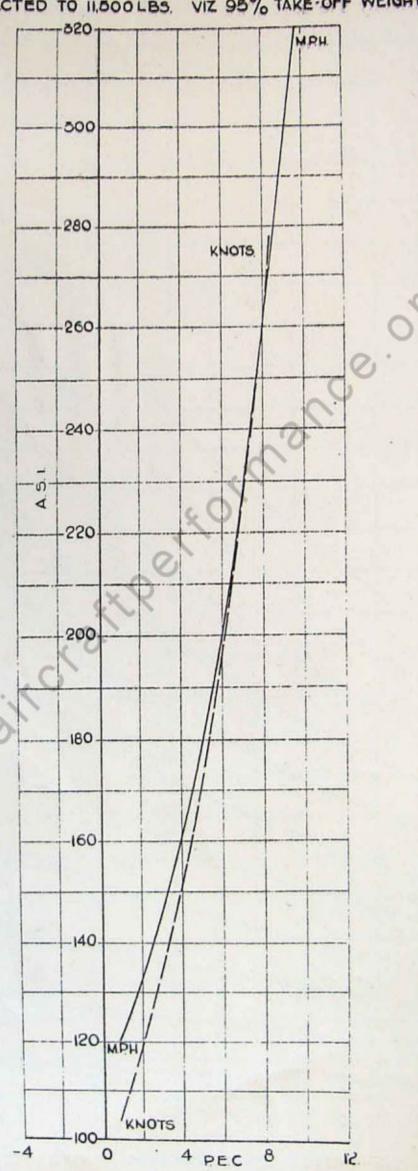




TYPE OF PRESSURE HEAD KOLLSMAN AN 5816-2 24V MFRS PART Nº 3690-012 RATIO OF APERTURE CF TUBE TO EXTERNAL DIA OF STATIC TUBE ___ SEE SKETCH INCIDENCE OF MAIN PLANE (ADJACENT TO PRESSURE HEAD) ____ +20.05 A ANGLE OF HEAD TO CHORD OF MAIN PLANE ____ NOSE OF HEAD TO MAIN PLANE (MINIMUM DISTANCE)_____ " SUPPORTING STRUT______ CHORD LINE_ " M.P. LEADING EDGE (PARALLEL TO CHORD.)_____ 25 % C LENGTH OF CHORD AT SECTION _____ E STRUT TO VENTS (MEAN.) ______ M MAJOR AXIS OF STRUT______ N MINOR Y DISTANCE FROM PLANE OF SYMMETRY_ POSITION LEADING EDGE PORT MAIN PLANE SEMI SPAN RATIO OF THICKNESS TO CHORD OF AEROFOIL SECTION, ADJACENT TO PRESSURE HEAD.

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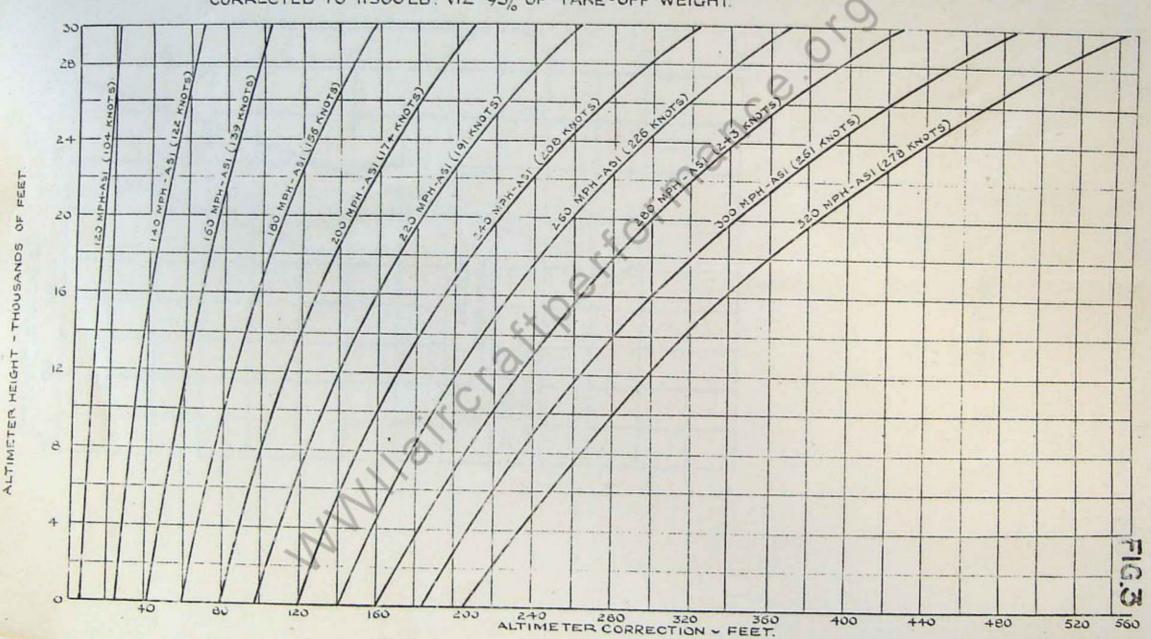
POSITION ERROR CORRECTION. (CORRECTED TO 11,500 LBS. VIZ 95% TAKE-OFF WEIGHT)



ALTIMETER CORRECTION.

APPROVED

CORRECTED TO 11500 LB. VIZ 95% OF TAKE-OFF WEIGHT.



LEVEL SPEED PERFORMANCE.

IN AUXILIARY HIGH SUPERCHARGER GEAR (WITH AND WITHOUT WATER INJECTION)

ENGINE COWLING GILLS ~ INTERCOOLER SHUTTER & OIL COOLER SHUTTER CLOSED.

CORRECTED TO 96 % TAKE~OFF WEIGHT VIZ~11500 LB

